#### **General Disclaimer**

### One or more of the Following Statements may affect this Document

- This document has been reproduced from the best copy furnished by the organizational source. It is being released in the interest of making available as much information as possible.
- This document may contain data, which exceeds the sheet parameters. It was furnished in this condition by the organizational source and is the best copy available.
- This document may contain tone-on-tone or color graphs, charts and/or pictures, which have been reproduced in black and white.
- This document is paginated as submitted by the original source.
- Portions of this document are not fully legible due to the historical nature of some
  of the material. However, it is the best reproduction available from the original
  submission.

#### MCDONNELL LJUGLAS TECHNICAL SERVICES CO.

#### SPACE SHUTTLE ENGINEERING AND OPERATIONS SUPPORT

1.3-DN-C0504-036.

ORBITER TO SPACELAB ELECTRICAL POWER INTERFACE

#### AVIONICS SYSTEM ENGINEERING

30 JUNE 1976

This Design Note is Submitted to NASA Under Task Order No. CO504, in Fulfillment of Contract NAS 9-14960.

PREPARED BY:

E. Emmons

Senior Engineer

488-5660 Ext. 285

APPROVED BY:

Séhior Group Engineer

188-5660 Ext. 265

APPROVED BY:

Technical Manager

483-5660 Ext. 261

Pannett

Project Manager

488-5660 Ext. 258

(NASA-CR-147834) SPACE SHUTTLE ENGINEERING AND OPERATIONS SUPPORT. ORBITER TO SPACELAB ELECTRICAL POWER INTERFACE. AVIONICS SYSTEM ENGINEERING (McDonnell-Douglas Astronautics) ንዓ <sub>ከ</sub> ዘሮ ቁዟ.በሰ

N76-28340

Unclas

#### 1.0 .SUMMARY

This report presents the results of an investigation of the factors which affect the determination of Spacelab (S/L) minimum interface Main DC voltage and available power from the Orbiter. This study addresses the dedicated fuel cell mode of powering the S/L and identifies the minimum S/L interface voltage and available power using the predicted fuel cell power plant performance curves. The values obtained are slightly lower than current estimates and represent a more marginal operating condition than previously estimated.

#### 2.0 DISCUSSION

Figure 1 is a simplified diagram of the Orbiter to Spacelab Main DC power feeder depicting the dedicated fuel cell configuration for the S/L Large Module (LM). In this mode the S/L receives its power from fuel cell No. 3 via Orbiter Main DC bus C. The resistances shown represents Rockwell furnished data and are for 1/0 gauge wire at 68 °F.

The key factors affecting the voltage and power available to the S/L are fuel cell performance and feeder line resistance. The following discussion deals with those variables affecting fuel cell performance and feeder line resistance and their affect on determination of minimum S/L voltage and available power.

### 2.1 Fuel Cell Performance

One of the prime concerns of this study is to identify worst-case or marginal performance aspects. For this reason the fuel cell performance characteristics for a 5000 hour fuel cell are used. Figure 2 depicts the performance curves for both steady state and transient conditions. The transient curves shown depict the predicted minimum fuel cell output voltage for step load changes. Figure 3 is a plot of step load changes to 12KW versus minimum transient voltage. The maximum step load change is 10KW and would represent a change in load demand from the steady state operating point of 2KW to 12KW. This curve was constructed

by plotting additional transient curves for steady state operating points to 12KW. An example is shown in Figure 2 for a step load change of 5KW from 7KW to 12KW. No data exists which describes transient to steady recovery time. It is the opinion of R/SD and NASA engineers that recovery to steady state occurs within 5 to 7 minutes. For purposes of this study it is assumed that recovery to steady state occurs in 7 minutes and is linear.

#### 2.2 Feed Resistance

Figure 1 indicates the S/L Main feeder line resistance for 1/0 gauge wire at  $68^{\circ}F$  and the longest feeder line (25 ft. for the S/L, L/M configuration). Factors affecting line resistance which must be considered in a worst case analysis are ambient wire temperature and increases in wire temperature due to  $I^2R$  heat build up.

### 2.2.1 Ambient Temperature

The payload bay wire tray ambient temperature will vary due to vehicle orientation as defined in Shuttle Vehicle to S/L ECLSS/Thermal Interfaces, ICD-2-05201.

This temperature can range from -280°F to +200°F in orbit. For purposes of this study the resistance of the components and wire in the Main Power Distrubution Assembly was considered to remain at ambient temperature. This unit is mounted on a cold plate.

### 2.2.2 Line Loss Heating

Figure 4 is a curve showing steady state temperature versus current for a I/O gauge wire of the type used in the S/L feeder circuit. This data is from the R/SD laboratory test report LTR 1705-7801 dated October 27, 1975, "Space Shuttle Temperature/Current Characteristics of Connectors - Evaluation Test." Laboratory test conditions simulated those which the feeder line will encounter in space. Of more significance to this evaluation is the rate of wire temperature increase, since the fuel cell performance requirements limits the maximum time at 12KW to 15 minutes every three hours; the maximum temperature the wire will reach will be

limited by this time factor. Figure 5 is a curve extrapolated from the R/SD test report which shows rate of temperature increase of a 1/0 gauge wire carrying 200 During the first 15 minutes the temperature increases at a rate of approximately 6.5 degrees per minute. This test was performed at 250°F. Each conductor in circuit segment 1 in Figure 1 will carry slightly over 200 amps at Therefore the 6.5 degree rate of temperature increase is applied for Segment In Circuit Segment 2 each conductor will carry half the current of segment 1 or one forth the power; therefore the temperature of this segment will increase at approximately one forth of the rate of Segment 1, or 1.625 degrees per minute. In summary the feeder line resistance will vary as a function of ambient temperature and wire temperature due to feeder line current. Wiring heating due to line current is a function of time with the maximum temperature for this analysis occurring 15 minutes after initiation of a step load change. This is an importent factor to consider in determining maximum available power to the spacelab.

Results

Appendix 1 presents an explanation of the calculations performed in this study and includes calculated data for various values of step load change ( $\Delta$  P) and ambient temperature. Figures 6, 7, and 8 are plots of data contained in Appendix I which represent selected operating conditions which are intended to provide performance references and indicate worst case performance.

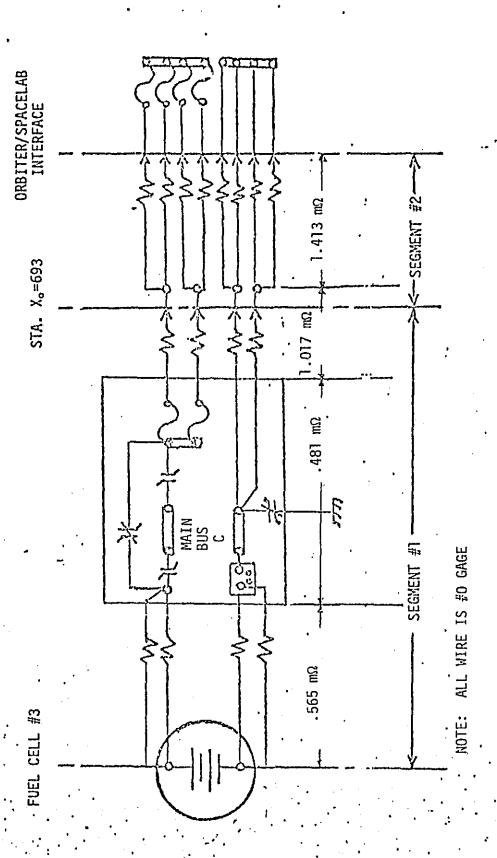
Figure 6 is a plot of step load change vs minimum S/L interface voltage for an ambient temperature of 68°F. Minimum interface voltage occurs for a ΔP of 10KW at an ambient wire temperature of 200°F. The minimum voltage under these conditions is 25.6 volts.

Figure 7 is a plot of minimum interface voltage vs ambient temperature for ΔP of 5KW and 10KW. The ΔP = 5KW curve represents performance for step load change from fuel cell maximum continuous output (7KW) to fuel cell peak output (12KW). From 70° to 200°F the interface voltage decreases approximately 0.35 volts.

Figure 8 is a plot of available interface power vs wire tray temperature. This curve is the minimum power available to the S/L during the 15 minute peak load period for a ΔP of lOKW and varies from 11.33 KW to 11.19 KW over the full range of ambient temperatures.

### 3.0 CONCLUSION: "ND RECOMMENDATIONS

It is the conclusion of this study that in using the predicted fuel cell performance curves for a 5000 hour fuel cell the minimum S/L interface voltage is 25.6 volts. This will occur at an ambient temperature of 200°F for a step load change from 2KW to 12KW. The minimum peak power available will be 11,150 watts. These "predicted" levels are somewhat lower than previous estimates and represent more marginal operating conditions than previously anticipated. The present values in ICD-2-0301, Shuttle Vehicle/Spacelab Avionics Interfaces are "26.4" volts and "12 KW peak minus losses". As fuel cell development tests are completed the data will be reflected in updated performance curves. It is expected that this data will be available in September or October of this year. Unless development testing indicates fuel cell rarformance to be considerably better than predicted, some operational constraints may have to be employed. These could range from supporting Spacelab flights with "new" fuel cells only, to restricting step load changes when using "old" fuel cells. As more accurate fuel cell performance data becomes available it is recommended than in in-depth study be performed to determine the minimum voltage and peak power available to the Spacelab and if required identify the action necessary to being these parameters within an acceptable operating range.



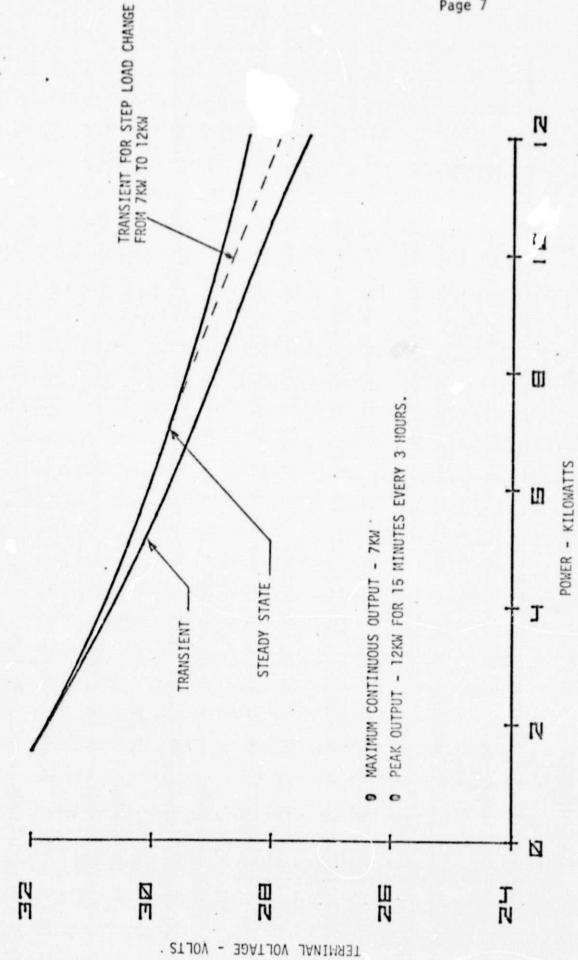
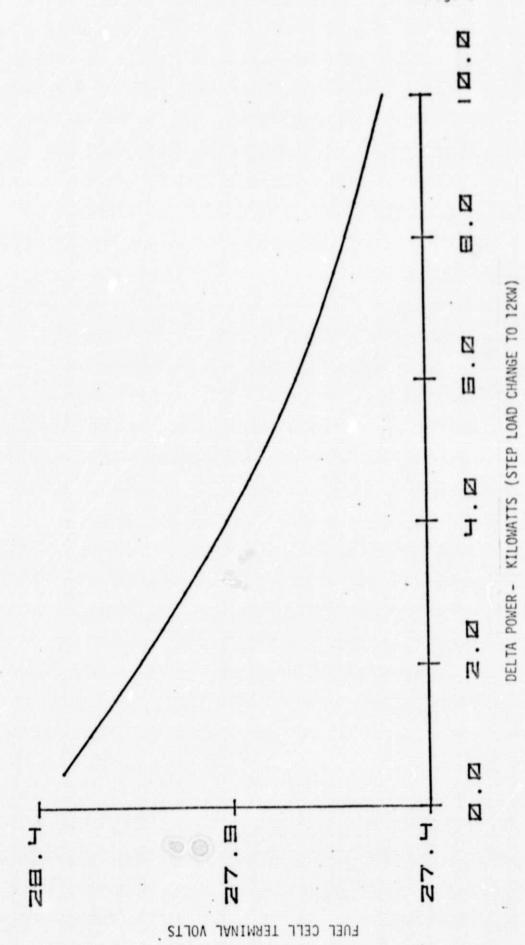


FIGURE 2: PREDICTED FUEL CELL POWER PLANT PERFORMANCE



MINIMUM FUEL CELL VOLTAGE VS STEP LOAD CHANGE TO 12KM FIGURE 3:

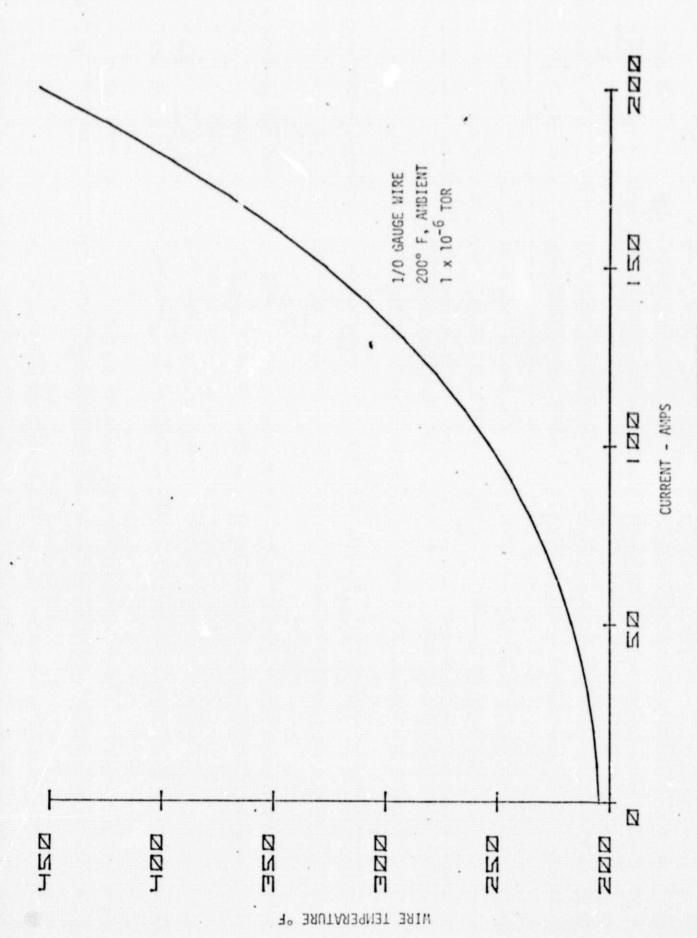


FIGURE 4: CURRENT VS STEADY TEMPERATURE

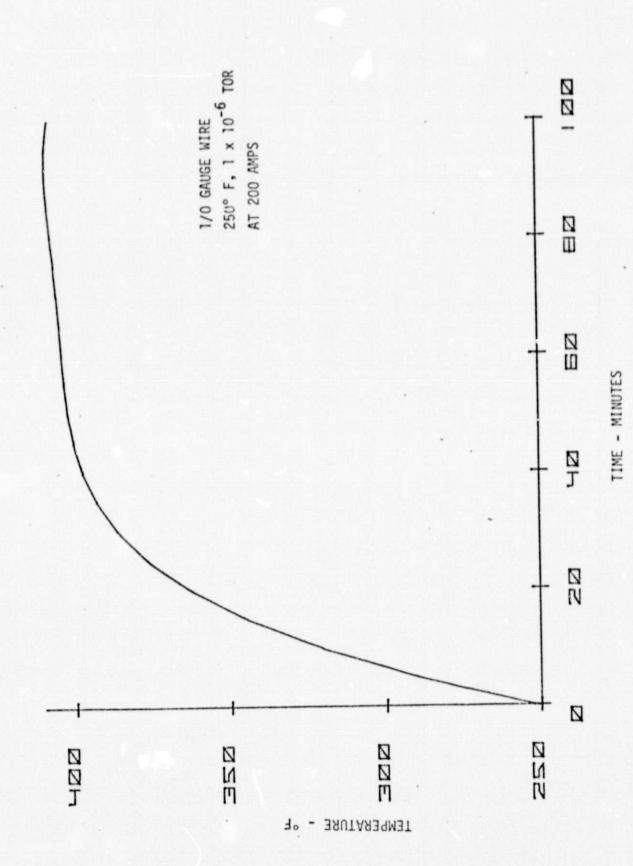
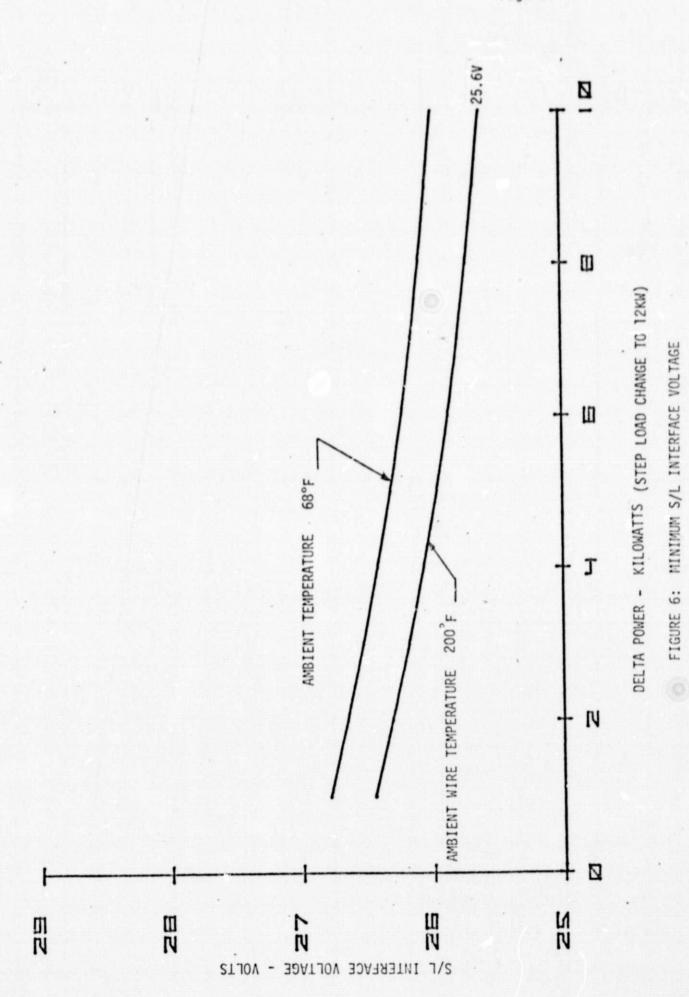


FIGURE 5: TEMPERATURE RISE TIME FOR 1/0 GAUGE WIRE CARRYING 200 AMPS



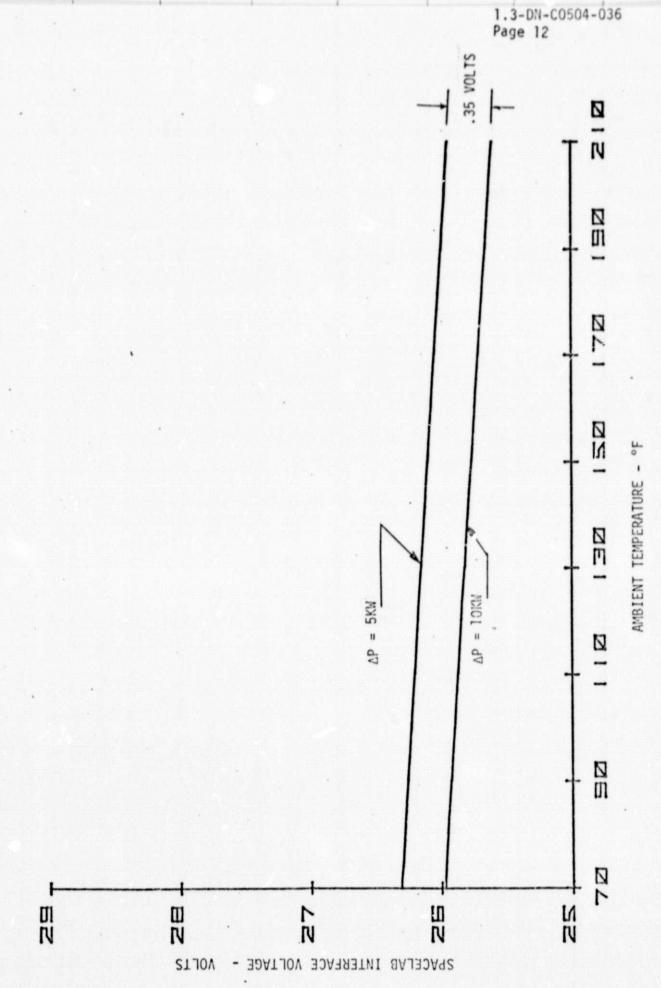


FIGURE 7: MINIMUM S/L INTERFACE VOLTAGE VS AKSIENT TEMPERATURE

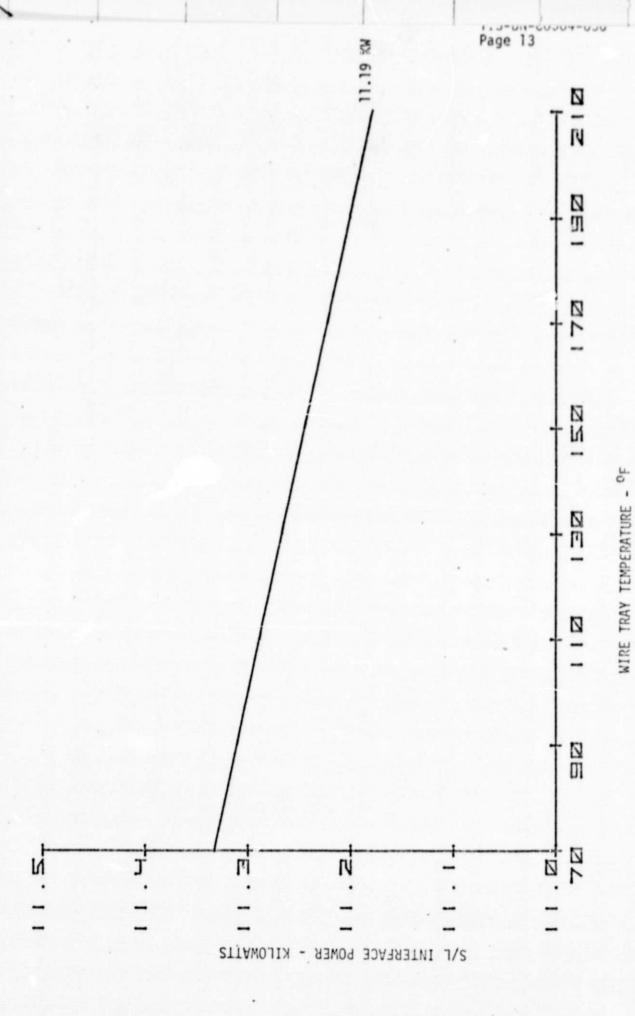


FIGURE 8: MAXIMUM USEFUL POWER TO S/L AT PEAK FÜEL CELL OUTPUT

## APPENDIX I

ORBITER TO SPACELAB ELECTRICAL POWER INTERFACE CALCULATIONS AND DATA

#### OBJECTIVES

- o To define S/L interface voltage as a function of a change in load demand.

  This takes into account the effects of the fuel cell thermal transient characteristic.
- o To determine the minimum useful power at the Orbiter/Spacelab interface.

### Fuel Cell Terminal Voltage

o The following expression is obtained from construction and "curve fit" from the predicted Fuel Cell performance curves:

$$V_{FCmin} = 28.4 - .1307 \Delta P + .00107 \Delta P^2 + .001029 \Delta P^3 - .0000516 \Delta P^4$$

VFCmin - Minimum fuel cell transient voltage at 12KW

Δ P - Step load change to 12KW

o The following expression defines the fuel cell terminal voltage as a function of time (thermal recovery to steady state in 7 min):

$$V_{FC} = V_{FC min} + \frac{(28.4 - V_{FC min})}{7}$$
 t

V<sub>FC</sub> - Fuel cell terminal voltage

 $V_{FC\ min}$  - Minimum fuel cell transient voltage at 12KW

t = Time in minutes (Limited to 7 minutes)

### Fuel Cell Current

$$I_{FC} = 12000/V_{FC}$$

I<sub>FC</sub> = Fuel Cell output current at 12KW

 $V_{FC}$  - Fuel Cell terminal voltage

### Wire Resistance (From Figure 1)

RT = Resistance of Thermally controlled segment, + resistance of 2 wire segment as a function of ambient temperature and temperature increase due to line current, + resistance of 4 wire segment as a function of ambient temperature and temperature increase due to line current.

$$R_T = [.481 + (.565 + 1.017)[1 + K (T_A + 6.5t - 68)] + 1.413 [1 + K(T_A = 3.25t - 68)]] \times 10^{-3}$$

R<sub>T</sub> - Feeder Resistance

 $T_{\Lambda}$  - Ambient Temperature

t - Time in minutes (limited to 15 minutes at 12KK)

K - Temperature coefficient of resistance. (.002055 mΩ/°F)

This reduces to:

$$R_T = (3.058 + .00615 T_A + .0164t) 10^{-3}$$

# S/L Interface Voltage

V<sub>IF</sub> = V<sub>FC</sub> - I<sub>FC</sub> R<sub>T</sub>

·V<sub>IF</sub> - Spacelab Interface Voltage

V<sub>FC</sub> - Fuel Cell terminal voltage

I<sub>FC</sub> - Fuel Cell current

R<sub>T</sub> - Feeder resistance

### Interface Power

 $P_{IF} = 12000 - I_{FC}^{2} R_{T}$ 

P<sub>lF</sub> - Power avaiable to Spacelab

IFC - Fuel Cell current

R<sub>T</sub> - Feeder resistance

## Procedure

Given the step load change ( $\Delta$  P) the above equations are solved for P $_{
m IF}$  and V $_{
m IF}$  for various values of ambient temperature. The resulting data is enclosed.

T TEMPERATURE 6: PIF 11374 11374 11374 11374 11369 11363 113
--

DELTA TIME 1 2 3 4 5 6 7 8 9 0 1 1 2 1 3 1 4 1 5 1 4 1 5	P 4, AMBI VIF 26.417 26.484 26.550 26.683 26.683 26.862 26.862 26.855 26.848 26.834 26.837	ENT TEMPER IFC 93.86 428.89 428.79 426.79 425.62 422.54 422.54 422.54 422.54 422.54 422.54 422.54	ATURE PIF 11358 11358 1358 1358 11358 11358 11358 11358 11358 11358 11358 11358 11358 11358 11358 11358	68		
DELTA TIME 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	P 5, AMB VIF 26.315 26.396 26.477 26.558 26.559 26.883 26.862 26.862 26.855 26.855 26.848 26.841 26.834 26.834	IENT TEMPER 150.42 431.42 438.84 428.54 426.84 426.84 422.54 422.54 422.54 422.54 422.54 422.54 422.54 422.54	RATURE PIF 11353 11354 11355 11356 11357 11358 11359 11359 11359 11344 11344 11335	68		
DELTA TIME 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	P 6, AMB VIF 26.227 26.321 26.415 26.508 26.695 26.895 26.862 26.862 26.841 26.834 26.834	IENT TEMPE 1FC 72 432.72 431.76 429.29 428.29 428.54 422.54 422.54 422.54 422.54 422.54 422.54	RATURE PIF 11349 11351 11352 11353 11355 11356 11358 11347 11344 11343 11335	68	ORIGINAL PAGE I OF POOR QUALIT	IN IN

			,
DELTA F TIME 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	VIF 26.153 26.257 26.361 26.465 26.570 26.674 26.778 26.883 26.876 26.869 26.862 26.855 26.848 26.848	422.54 11347 422.54 11344 422.54 11344 422.54 11338	68
DELTA F TIME 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	VIF 26.089 26.202 26.316 26.429 26.542 26.656 26.769 26.883 26.876 26.869 26.862 26.855	ENT TEMPERATURE IFC PIF 434.78 11343 432.98 11345 431.21 11348 429.44 11350 427.70 11352 425.96 11354 424.24 11357 422.54 11356 422.54 11356 422.54 11353 422.54 11344 422.54 11347 422.54 11344 422.54 11338 422.54 11338	68
DELTA I TIME 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	9, AMBI VIF 26.033 26.155 26.276 26.397 26.519 26.640 26.869 26.869 26.869 26.862 26.862 26.862 26.862 26.855 26.848 26.841 26.834 26.827	ENT TEMPERATURE IFC PIF 435.61 11340 433.69 11343 431.79 11346 429.91 11351 426.19 11351 426.19 11354 424.35 11356 422.54 11356 422.54 11353 422.54 11353 422.54 11344 422.54 11347 422.54 11347 422.54 11344 422.54 11338 422.54 11338	68

ORIGINAL PAGE IS OF POOR QUALITY

DELTA P TIME 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	1, AMB: VIF 26.448 26.461 26.474 26.500 26.513 26.527 26.533 26.536 26.536 26.519 26.512 26.519 26.498 26.491 26.484	IENT TEMPER IFC 424.51 424.22 423.94 423.66 423.38 423.10 422.54 422.54 422.54 422.54 422.54 422.54 422.54 422.54 422.54 422.54 422.54	RATURE 200 PIF 11227 11225 11223 11222 11220 11218 11216 11214 11211 11208 11208 11209 11199 11199 11196 11190
DELTA F TIME 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	2, AMB VIF 26.312 26.345 26.377 26.410 26.475 26.507 26.507 26.533 26.526 26.519 26.512 26.498 26.491 26.484	IENT TEMPE  IFC  426.43 425.87 425.31 424.75 424.19 423.64 423.54 422.54 422.54 422.54 422.54 422.54 422.54 422.54 422.54	RATURE 200 PIF 11220 11219 11218 11217 11216 11215 11214 11211 11208 11208 11205 11202 11196 11196 11190

DELTA TIME 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	P	3, AM VIF 26.185 26.286 26.387 26.387 26.489 26.538 26.538 26.538 26.549 26.519 26.505 26.491 26.491 26.491	422.54 422.54	RATURE 200 PIF 11214 11214 11214 11214 11214 11214 11214 11214 11219 11208 11208 11208 11208 11208 11208 11208
DELTA TIME 0 1 23456789 10112314 15	F	4, AN VIF 26.068 26.136 26.270 26.270 26.338 26.472 26.526 26.519 26.519 26.491 26.491 26.491	427.79 426.73 426.62 423.58 422.54 422.54 422.54 422.54 422.54	RATURE 200 PIF 11207 11208 11209 11210 11212 11212 11213 11214 11208 11208 11208 11208 11208 11208 11208 11208 11208
DELTA TIME 1 23456789 112314 15	P	5, AN VIF 25.965 26.047 26.129 26.211 26.293 26.540 26.533 26.519 26.519 26.491 26.491 26.494	425.04 423.78 422.54 422.54 422.54 422.54 422.54	RATURE 200 PIF 11202 11204 11205 11207 11209 11211 11212 11214 11208 11208 11205 11208 11190 11190

ORIGINAL PAGE IS OF POOR QUALITY

DELTA TIME .0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	6, AMB VIF 25.876 25.971 26.066 26.160 26.255 26.350 26.533 26.533 26.526 26.519 26.512 26.408 26.471 26.484	IENT TEMPE IFC 432.72 431.23 429.76 428.29 426.84 425.40 423.96 422.54 422.54 422.54 422.54 422.54 422.54 422.54 422.54 422.54 422.54 422.54	11199 11196 11193
DELTA TIME 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	7, AMB VIF 25.800 25.906 26.012 26.117 26.223 26.328 26.540 26.533 26.536 26.519 26.512 26.505 26.498 26.491 26.484	IENT TEMPE IFC 433.83 432.18 430.54 428.92 427.30 425.70 424.11 422.54 422.54 422.54 422.54 422.54 422.54 422.54 422.54 422.54 422.54 422.54	RATURE 200 PIF 11193 11196 11199 11202 11205 11208 11211 11214 11214 11211 11208 11205 11205 11205 11206 11199 11196 11190
DELTA TIME 0	8, \AMB VIF 25.736	IENT TEMPER IFC 434.78	RATURE 200 PIF 11189

DELTA	P					RATURE	200
TIME		VIF		IFC		PIF	
0		25.7			.78	11189	
1		25.8	351	432	.98	11193	3
2		25.9	966	431	.21	11197	7
1 2 3 4		26.6	180	429	.44	11200	3
4		26.1			7.70	11204	
5		26.3			.96	11207	
		26.4			.24	11211	
6789		26.5			.54	11214	
0		26.5					
0					.54	11211	
		26.5		422	.54	11208	
10		26.5	119	422	.54	11205	5
11		26.5	12	422	.54	11202	2
12		26.5	05		.54	11199	
13		26.4			.54	11196	
14		26.4			.54	11193	
15		26.4	Control of the contro		.54	11190	

DELTA	P	9,	AMBIE	EHT	TEMPE	RATURE 200
TIME		VIF		IF(	3	bīk
9.		.25.6	89	435	5.61	11186
1		25.8	ប្ទ	430	3.69	11190
2		25.9	25	430	1.79	11194
3		26.0	48	429	9.9i	11198
4		26.1	71	42	3,04	11202
23456789		26.2	94	420	5.19	11206
6		26.4		42	4.35	11210
7		26.5	40	42:	2.54	11214
8		26.5	33		2.54	11211
9		26.5	26	42:	2.54	11208
10		26.5			2.54	11205
11		26.5			2.54	11202
12		26.5			2.54	11199
13		26.4	98		2.54	11196
14		26.4	91		2.54	11193
15		26.4	84	42:	2.54	11190

DELTA	F	10,	AMB I			ERATU		200
TIME		VIF		IFO		PΙ		
ė ·		25.62	27	4.36	. 40	11	183	
		25.75	57	434	1.36	11	188	<b>)</b>
1 2		25.88		433	2.34	11	192	2
3		26.01			3.35		197	
4.		26.14			3.37		201	
5		26.27			40		205	
<u>ل</u> -							210	
6 7		26.48		-	4.46			
7		26.5			2.54		214	
8		26.50	33	423	2.54	11	211	l
8 9		26.53	26	422	2.54	11	208	}
10		26.5			2.54	11	205	5
īī		26.5			2.54	11	202	2
iż		26.50			2.54		199	
îŝ		26.49			2.54		196	
		26.4			2.54		190	
14								
15		26.40	54	427	2.54	11	190	9

DELTA P TIME 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	5, AN VIF 26.310 26.391 26.472 26.553 26.634 26.715 26.877 26.877 26.871 26.857 26.857 26.858 26.836 26.836 26.836 26.836		70
DELTA P TIME 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	5; At VIF 26.284 26.365 26.446 26.527 26.608 26.689 26.770 26.851 26.838 26.831 26.831 26.824 26.817 26.810 26.796	430.13 11340 428.84 11341 427.57 11342 426.30 11343 425.04 11344 423.78 11345 422.54 11346 422.54 11343 422.54 11340 422.54 11337	80
DELTA P TIME 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	5, At VIF 26.231 26.312 26.393 26.474 26.556 26.799 26.799 26.793 26.772 26.765 26.758 26.758 26.758 26.751 26.744	MBIENT TEMPERATURE  IFC PIF  431.42 11316  430.13 11317  428.84 11318  427.57 11320  426.30 11321  425.04 11322  423.78 11323  422.54 11324  422.54 11318  422.54 11318  422.54 11318  422.54 11318  422.54 11300  422.54 11300	100

DELTA TIME 0 123456789011213145		5, All 7790 VIF 1790 26.340 26.403 26.586 26.741 26.720 26.720 26.720 26.720 26.720 26.720 26.720 26.720 26.720 26.720	MBIEHT T 1FC 430. 420. 422. 422. 422. 422. 422. 422. 422. 422.	13 11 84 11 57 11 90 11 78 11 78 11 54 11 54 11 54 11 54 11 54 11	F 293 295 296
DELTA TIME 0 1 234567890112311211311415	P	5; All VIF 124 26.288 26.289 26.389 26.389 26.689 26.689 26.689 26.689 26.684 26.684 26.684 26.684 26.684 26.684 26.684 26.884 2	150. 430. 430. 422. 422. 422. 422. 422. 422. 422.	13 11 84 11 57 11 30 11 04 11 78 11 54 11 54 11 54 11 54 11 54 11	

DELTA	Ρ	5,	AMBI			ERAŢŲŖE	160
TIME		VIF		IFC		PIF	
Ø		26.07	71	431	.42	11248	}
1		26,13	53	436	).i3	11249	)
123456		26.20	35		8.84	11251	
3		26.3			7.57	11252	
4							
4		26.39			.30	11254	
Þ		26.48			i. 84	11255	
		26.56	52	423	78	11256	,
7		26.64	14	423	54	11258	}
7 8 9		26.63			.54	11255	
9		26.63	30	423	54	11252	<u>)</u>
10		26.63			.54	11249	
11		26.6			.54	11246	
12		26.69	39		.54.	11243	}
13		26.60			.54		
14		26.59			.54	11237	
Ī5		26.58			.54	11234	
10			- · · · ·	766		11407	ī

JELTA JIME	VIF	BIENT TEMP	ERATURE 180 PIF
0 1	26.018 26.100	431.42 430.13	11225 11226
1 2 3 4 5 6 7 8 9 9	26.100 26.182 26.264	428.84 427.57	11228 11230
5	26.346 26.428 26.510 26.592	426.30 425.04 422 70	11231 11233 11234
7 8	26.592 26.585	423.78 422.54 422.54	11236
9 10	26, 578	422.54 422.54	11230 11227
11	26.571 26.564 26.557	422.54 422.54	11224 11221
13 14	26.550 26.543	422.54 422.54	11218 11215
15.	26.536	422.54	11212
DELTA TIME	P 5, AME	SIENT TEMPE	
TIME	VIF 25.965	IFC 431.42	PIF 11202
TIME	VIF 25.965 26.847 26.129 26.211	IFC 431.42 430.13 428.84 427.57	PIF 11202 11204 11205
TIME	VIF 25.965 26.047 26.129 26.211	IFC 431.42 430.13 428.84 427.57 426.30 425.04	PIF 11202 11204 11205 11207 11209 11211
TIME	VIF 25.965 26.047 26.129 26.211	IFC 431.42 430.13 428.84 427.57 426.30 423.78 422.54	PIF 11202 11204 11205 11207 11209 11211 11212 11214
TIME 0 1 2 3 4 5 6 7 8	VIF 25.965 26.047 26.129 26.211	IFC 431.42 430.13 428.84 427.57 426.30 425.78 422.54 422.54 422.54	PIF 11202 11204 11205 11207 11209 11211 11212 11214 11211 11208
TIME 0 123456789011	VIF 25.965 26.047 26.129 26.211	IFC 421.13 430.13 430.57 422.30 422.54 422.54 422.54 422.54 422.54	PIF 11202 11204 11205 11207 11209 11211 11212 11214 11208 11205 11202
TIME 0 1 2 3 4 5 6 7 8 9 10	VIF 25.965 26.847 26.129 26.211	IFC 431.42 430.13 428.84 427.50 425.94 423.54 422.54 422.54 422.54	PIF 11202 11204 11205 11207 11209 11211 11212 11214 11211 11208 11205

ORIGINAL PAGE IS OF POOR QUALITY

TIME 1 2 3 4 5 6	VIF 25.60 25.90 25.90	30 11 11 31 31 31 35 35 35 37 37 37	156420006423333344444444444444444444444444	486457064444444444444444444444444444444444	PIF 11207 11211 11225 11226 11226 11236 11236 11227 11227	; ; ; ; ; ; ; ; ; ; ; ;
11	26.5	54 57 50 43	422 422 422 423	54	11224	1 1 3 5

DELTA :	P	10,	AMBIE	ENT	TEMP	ERATU	RE	200
TIME		VIF		IFC		F'I	F	
Ø		25.62	27	436	40		183	
1		25.75	57	434	1.36		188	
2		25.88	88	432	2.34		192	
3		26,81	8	439	3.35	11	197	1
4		26.14	18	428	3.37	11	20 i	
234567		26.27	79	426	5.40	11	205	i
6		26.49	<del>1</del> 9	424	1.46	11	210	1
7		26.5		422	2.54	11	214	}
8		26.50		422	2.54	11	211	
ģ		26.53		422	2.54	11	206	)
10		26.5		422	2.54	11	205	j
īī		26.5		42:	2.54	11	202	2
īž		26.5		423	2.54	11	195	)
13		26,4		423	2.\54	11	196	5
14		26.4		42:	2.54	11	193	}
15		26.4		42:	2.54	11	198	j

```
AMBIENT TEMPERATURE 120
         10,
DELTA
                     IFC
436.40
                                 PIF
         VIF
TIME
                                 11277
         25,841
 Û
                     434.36
                                 11281
         25.971
 1
                                 11284
                     432.34
234567899
         26,100
                     439.35
                                 11288
         26,230
                                 11291
                     428.37
         26.359
                     426,40
                                  11295
         26.489
                                  11298
                     424.45
         26.618
                     422.54
         26.748
                                  11302
                     422.54
422.54
                                  11299
         26,741
                                  11296
         26.734
                                 11293
                      422.54
         26.727
                                  11298
         26.720
                      422.54
11
                      422.54
                                  11287
12
13
         26.713
                                  11284
                      422.54
          26.706
                                  11281
                      422.54
14
          26.699
                                  11278
                      422.54
          26.692
15
                AMBIENT TEMPERATURE 140
DELTH F
          10,
                                  PIF
                      IFC
          WIF
TIME .
                                  11254
                      436.49
          25.788
 Ü
                                  11258
                      434.36
          25.917
 1.
                                  11261
  234
          26,047
                      432.34
                      430.35
                                  11265
          26.177
                                  11269
          26.307
                      428.37
                                  11273
                      428,40
 56789
          26.436
                      424.46
                                  11276
          26.566
                                  11280
                      422.54
          26.696
                                  11277
                      422.54
          26.689
                                  11274
          25.682
                      422.54
                      422.54
                                  11271
 10
          26.675
11
                      422.54
                                  11268
          26.668
                                  11265
                      422.54
          26.661
 12
 13
                      422.54
                                   11262
          26.654
                                   11259
                      422.54
 14
          26.647
                      422.54
                                   11256
          26.648
 15
                AMBIENT TEMPERATURE 160
 DELTA P
          10,
                                   FIF
                       IFC
 TIME
          VIF
          25.734
                                   11230
                       436.40
  Ø
                                   11234
  1
          25.864
                       434.36
                                   112%是
  2
          25.994
                       432.34
                                   11242
                       430.35
          26.124
                       428.37
                                   11246
          26,254
  4
                                   11250
  56
           26,384
                       426.40
                                   11254
                       424.46
           26.514
                                                      ORIGINAL PAGE IS
  7
           26.644
                       422.54
                                   11258
                                                      OF POOR QUALITY
                       422.54
                                   11255
           26.637
  8
                                   11252
                       422.54
  9
           26.630
                                   11249
                       422.54
           26.623
 10
                       422.54
                                   11246
           26.616
 11
                                   11243
                       422.54
           26.609
 12
                                   11240
                       422.54
 10
           26.602
                                   11237
           26.595
                       422.54
 1.4
                                   11234
                       422.54
```

26.588

15

TIME 0 1 2 3 4 5 6 7 8 9 10 11 12 13		VIF 25.976 26.104 26.233 26.362 26.491 26.520 26.749 26.877 26.877 26.857 26.857 26.858 26.858 26.858	434.36 113 432.34 113 430.35 113 428.37 113 426.40 113 424.46 113 422.54 113 422.54 113 422.54 113 422.54 113 422.54 113 422.54 113 422.54 113 422.54 113	36 39 42 45 45 45 45 45 45 45 45 45 45 45 45 45
DELTA TIME 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15		10, AM VIF 25.949 26.078 26.207 26.336 26.465 26.594 26.723 26.851 26.845 26.838 26.831 26.831 26.817 26.810 26.803 26.796	434.36 113 432.34 113 430.35 113 428.37 113 426.40 113 424.46 113 422.54 113 422.54 113 422.54 113 422.54 113 422.54 113 422.54 113 422.54 113 422.54 113	24 27 30 33 40 43 46 43 40 31 32 31
DELTA TIME 0 1 2 3 4 5 5 7 8 9 10 11 12 13 14	P	10, AM VIF 25.895 26.024 26.154 26.283 26.412 26.541 26.799 26.799 26.793 26.772 26.765 26.758	BIENT TEMPERATUR  IFC PIF  436 40 113  434.36 113  432.34 113  430.35 113  428.37 113  426.40 113  424.46 113  422.54 113  422.54 113  422.54 113  422.54 113  422.54 113  422.54 113  422.54 113  422.54 113	01 04 07 11 14 17 21 24 21 18 15 12 09